

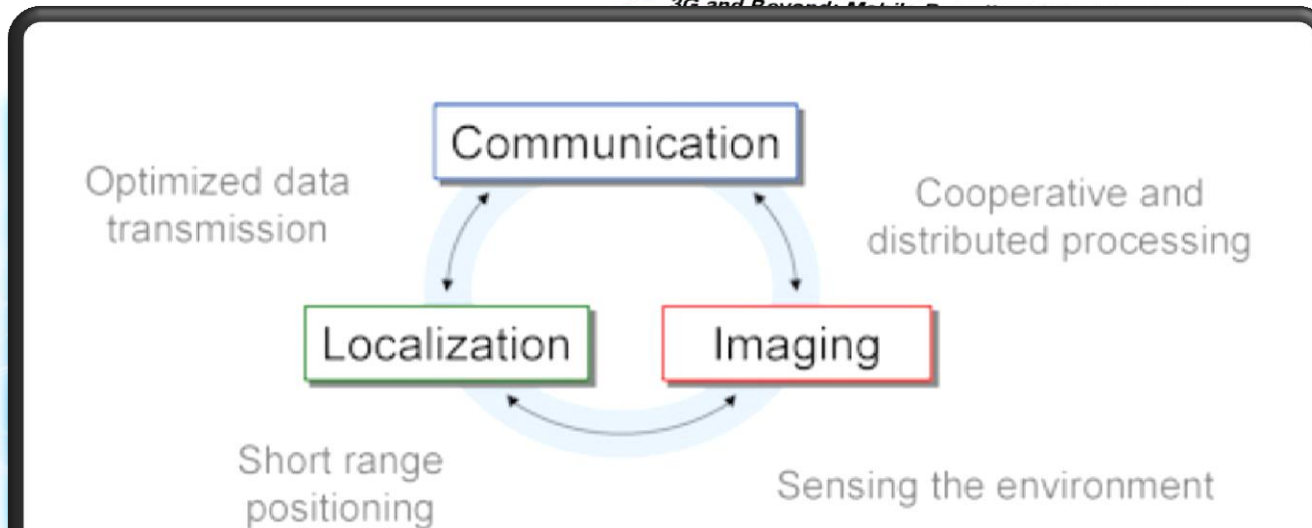
Wireless digital information transfer: modelling, prediction and assessment

Ioan E. Lager, Adrianus T. de Hoop, Delft University of Technology

Takamaro Kikkawa, Hiroshima University

19 March, 2013

The digital wireless-sphere



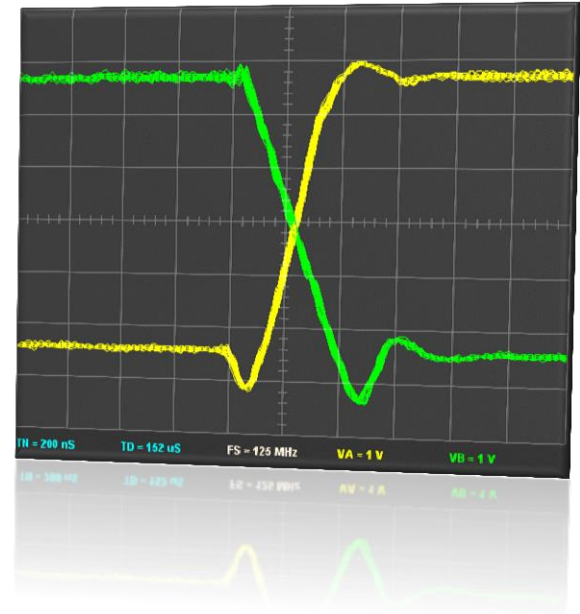
Wireless links' functionality:

- Are the signal levels involved sufficient for the proper system performance?
- Do the field emission levels comply with the (international) regulations on ElectroMagnetic Interference (EMI)?

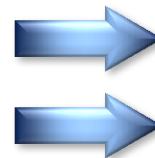
Synopsis

- Digital signals EMI analysis
- Prerequisites
 - analysed configuration
 - exciting pulses
 - theoretical background
- Loop-to-loop transfer
- Energy spectral density of the emitted field
- Numerical experiments
 - loop-to-loop transfer
 - energy spectral density of the emitted field
- Conclusions

Digital signals EMI analysis



- Digital electronic systems
- Their investigation

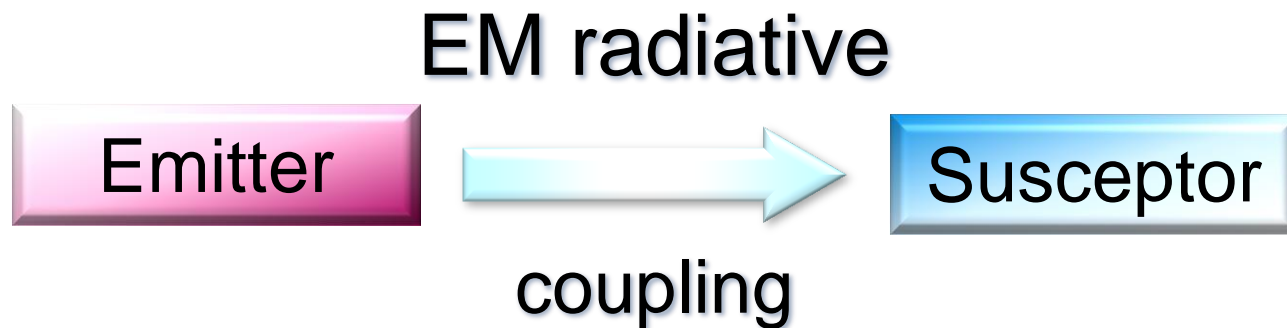


time-domain




time-domain

~~frequency-domain~~

Digital signals EMI analysis



The EMI triptych  its simplest representative circuit:

- **Transmitting loop**  pulsed electric current feeding
- **Receiving loop**  generator source of the equivalent Thévenin Kirchhoff circuit
- **Coupling path**  free space

Digital signals EMI analysis

- EM field description: the **time-domain** magnetic field H

compatibility 

- International EMI regulations: **frequency-domain** masks

Prerequisites: configuration

- Transmitting loop \mathcal{L}^T

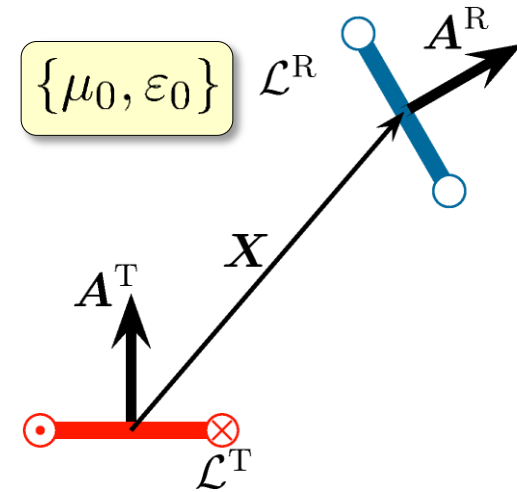
- reference centre: $\mathbf{x} = \mathbf{x}^T$

- area: $A^T = i_{A^T} A^T$

- Receiving loop \mathcal{L}^R

- reference centre: $\mathbf{x} = \mathbf{x}^R$

- area: $A^R = i_{A^R} A^R$



- Coupling path

- position: $X = \mathbf{x}^R - \mathbf{x}^T \Rightarrow X/|X| = \Xi$

- medium: free space $\{\epsilon_0, \mu_0\} \Rightarrow c_0 = (\epsilon_0 \mu_0)^{-1/2}$

Prerequisites: exciting pulses

Main requirement:

CAUSALITY

Prerequisites: exciting pulses

Time differentiated power exponential pulse (∂_t PE)

$$I(t) = I_{\text{peak}} N(\nu) \left(1 - \frac{t}{t_{0x}}\right) \left(\frac{t}{t_{0x}}\right)^{\nu-1} \exp\left[-\nu \left(\frac{t}{t_{0x}} - 1\right)\right] H(t) \text{ for } \nu > 1$$

where:

- I_{peak} = magnitude of the first peak in $I(t)$
- t_{0x} = pulse zero-crossing time (= t_r of the original PE)
- ν = initial rise power of the original PE
- $H(t)$ = Heaviside unit step function
- $N(\nu)$ = normalisation constant

$$N(\nu) = \nu^{1/2} \left(\frac{\nu^{1/2}}{\nu^{1/2} - 1}\right)^{\nu-1} \exp(-\nu^{1/2})$$

Prerequisites: exciting pulses

Time differentiated power exponential pulse (∂_t PE)

$$I(t) \xrightarrow{\text{LT}} \hat{I}(s)$$



$$\hat{I}(s) = I_{\text{peak}} t_{0x} N(\nu) \frac{s t_{0x} \Gamma(\nu) \exp(\nu)}{(s t_{0x} + \nu)^{\nu+1}} \text{ for } \text{Re}(s) > -\nu/t_{0x}$$

where:

– Γ = Euler gamma function



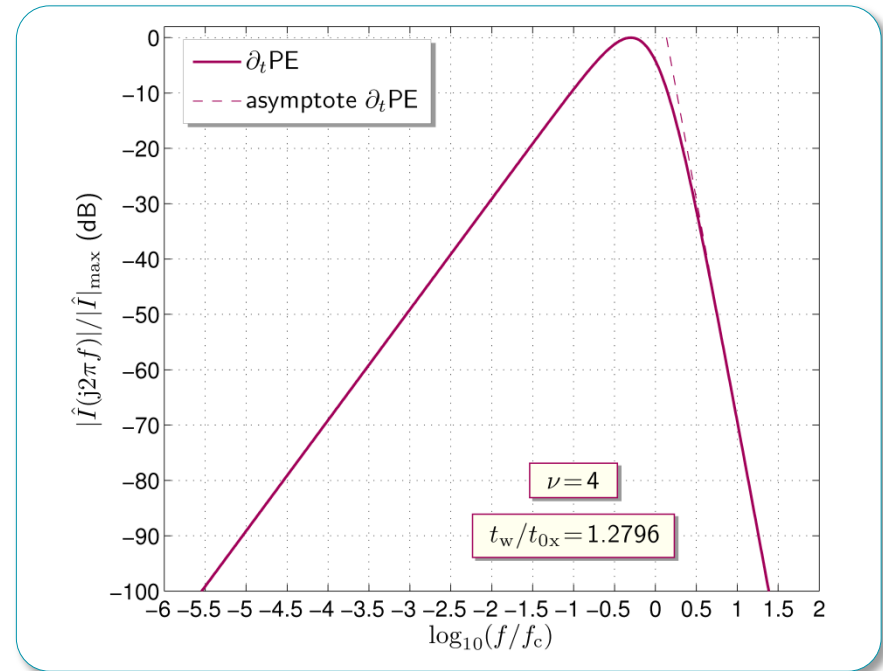
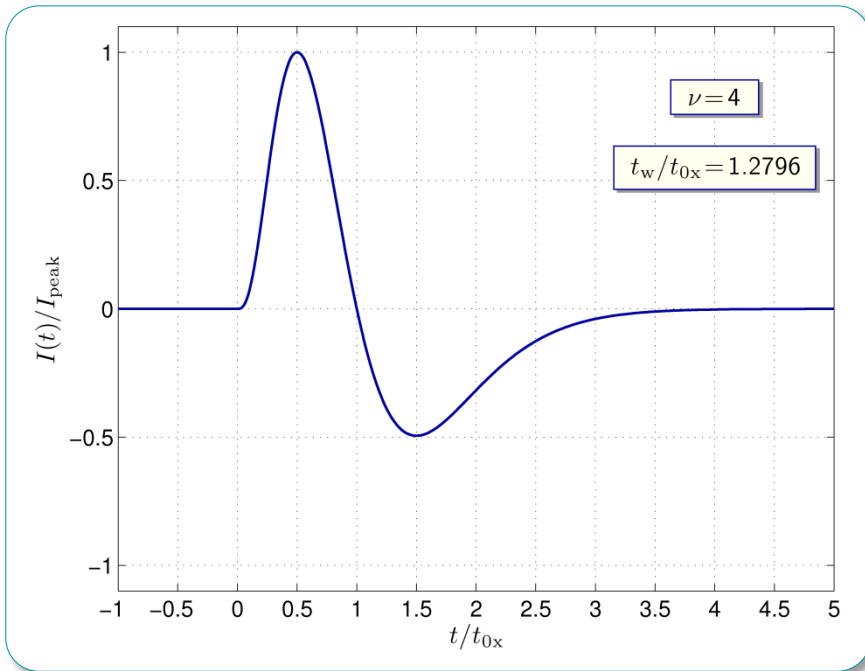
Fourier

$$I(t) \xrightarrow{\text{FT}} \hat{I}(j\omega) \longleftrightarrow s = j\omega = j2\pi f, \text{ with } \omega \in \mathbb{R}, f \in \mathbb{R}$$

Prerequisites: exciting pulses

Time differentiated power exponential pulse ($\partial_t \text{PE}$)

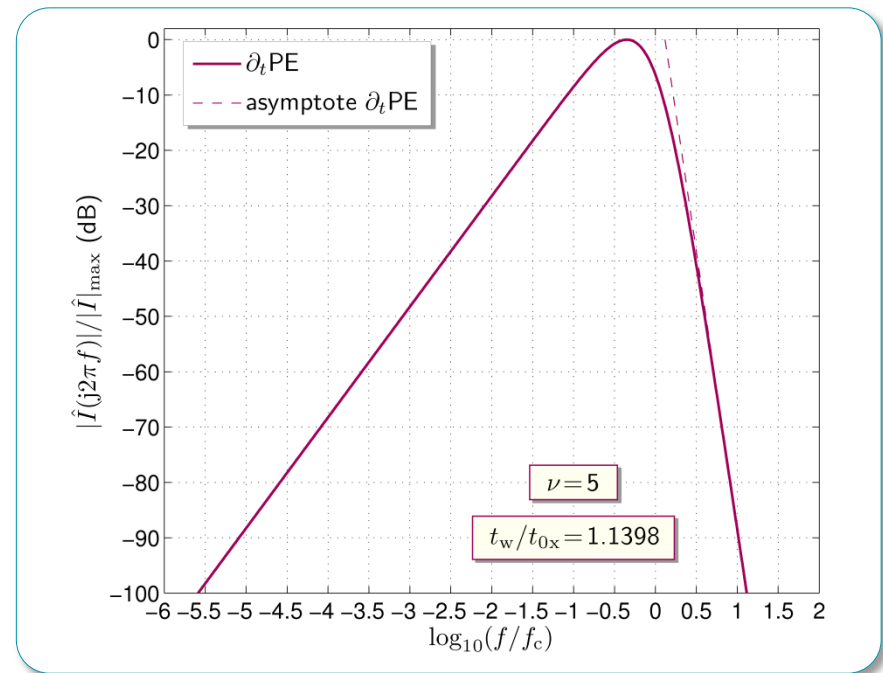
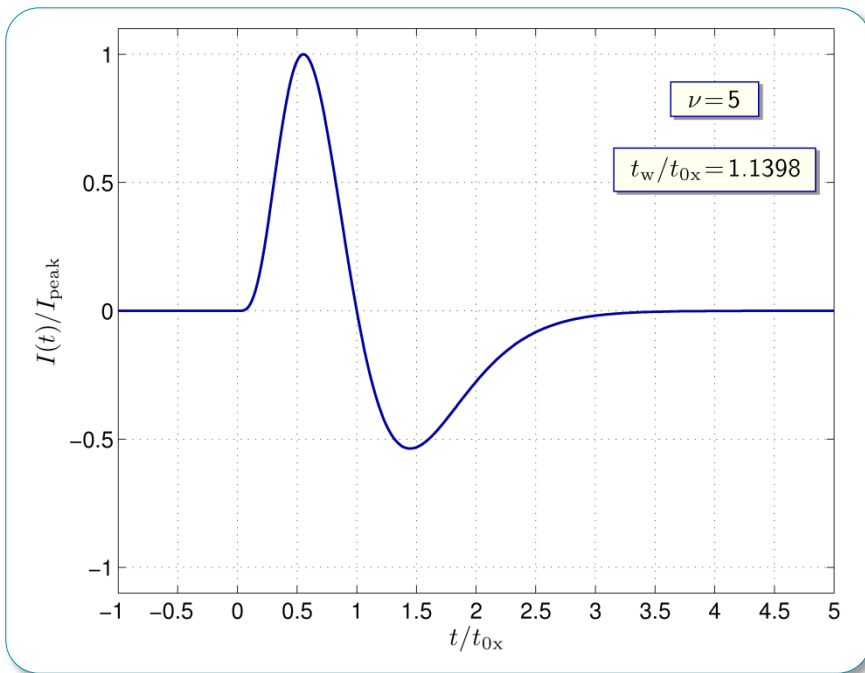
$$\nu = 4$$



Prerequisites: exciting pulses

Time differentiated power exponential pulse ($\partial_t \text{PE}$)

$$\nu = 5$$



Prerequisites: exciting pulses

Power exponential modulated – sinc-cosine pulse

- Normalised, unipolar, power exponential

$$I_{\text{PE}}(t) = I_0 (t/t_r)^\nu \exp[-\nu (t/t_r - 1)] H(t)$$

where:

- I_0 = pulse amplitude
- $t_r > 0$ = pulse rise time

- Sinc-cosine function

$$G(t) = \text{sinc}[B(t - t_0)] \cos[2\pi f_c(t - t_0)]$$

where:

- t_0 = arbitrary delay
- B = (prescribed) bandwidth $B = f_h - f_l$, with $0 < f_l < f_h$
- f_c = centre frequency $f_c = (f_l + f_h)/2$

Prerequisites: exciting pulses

Power exponential modulated – sinc-cosine pulse

- Normalised, unipolar, power exponential

$$I_{\text{PE}}(t) = I_0 (t/t_r)^\nu \exp[-\nu (t/t_r - 1)] H(t)$$

where:

- I_0 = pulse amplitude
- $t_r > 0$ = pulse rise time

- Sinc-cosine function

$$G(t) = \text{sinc}[B(t - t_0)] \cos[2\pi f_c(t - t_0)]$$

where:

- t_0 = arbitrary delay
- B = (prescribed) bandwidth $B = f_h - f_l$, with $0 < f_l < f_h$
- f_c = centre frequency $f_c = (f_l + f_h)/2$

non-causal

Prerequisites: exciting pulses

Power exponential modulated – sinc-cosine pulse

- Normalised, unipolar, power exponential

$$I_{\text{PE}}(t) = I_0 (t/t_r)^\nu \exp[-\nu (t/t_r - 1)] H(t)$$

causal

where:

- I_0 = pulse amplitude
- $t_r > 0$ = pulse rise time

- Sinc-cosine function

$$G(t) = \text{sinc}[B(t - t_0)] \cos[2\pi f_c(t - t_0)]$$

where:

- t_0 = arbitrary delay
- B = (prescribed) bandwidth $B = f_h - f_l$, with $0 < f_l < f_h$
- f_c = centre frequency $f_c = (f_l + f_h)/2$

non-causal

Prerequisites: exciting pulses

Power exponential modulated – sinc-cosine pulse

- Normalised, unipolar, power exponential (envelope)

$$I_{\text{PE}}(t) = I_0 (t/t_r)^\nu \exp[-\nu (t/t_r - 1)] H(t)$$

causal

where:

- I_0 = pulse amplitude
- $t_r > 0$ = pulse rise time

- Sinc-cosine function (carrier)

$$G(t) = \text{sinc}[B(t - t_0)] \cos[2\pi f_c(t - t_0)]$$

where:

- t_0 = arbitrary delay
- B = (prescribed) bandwidth $B = f_h - f_l$, with $0 < f_l < f_h$
- f_c = centre frequency $f_c = (f_l + f_h)/2$

non-causal

Prerequisites: exciting pulses

Power exponential modulated – sinc-cosine pulse

- By taking $t_0 = t_r$



$$I(t) = I_0 (t/t_r)^\nu \text{sinc} [B(t - t_r)] \cos [2\pi f_c(t - t_r)] \exp [-\nu (t/t_r - 1)] H(t)$$

- Choices:

- $\nu = 1, 2, 3, \dots$

- $B \leftrightarrow t_r$ as

$$t_r = K_{sc}/B, \text{ with } K_{sc} = 1, 2, 3, \dots$$

Prerequisites: exciting pulses

Power exponential modulated – sinc-cosine pulse

$$I(t) \xrightarrow{\text{FT}} \hat{I}(j\omega)$$



$$\begin{aligned}\hat{I}(j\omega) &= \frac{1}{2\pi} \left[\hat{I}_{\text{PE}}(j\omega) \overset{(j\omega)}{*} \hat{G}(j\omega) \right] \\ &= I_0 \frac{\exp(-j\omega t_r)}{4\pi B} [\mathcal{I}(\omega - \omega_h, \omega - \omega_l) + \mathcal{I}(\omega + \omega_l, \omega + \omega_h)]\end{aligned}$$

where:

– $\overset{(j\omega)}{*}$ = frequency convolution

Prerequisites: exciting pulses

Power exponential modulated – sinc-cosine pulse

$$I(t) \xrightarrow{\text{FT}} \hat{I}(j\omega)$$

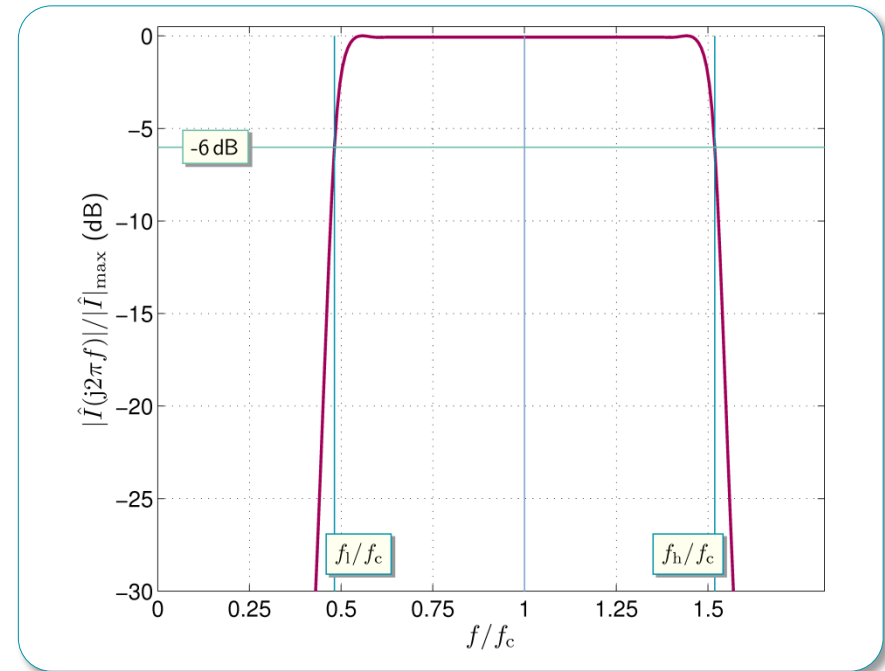
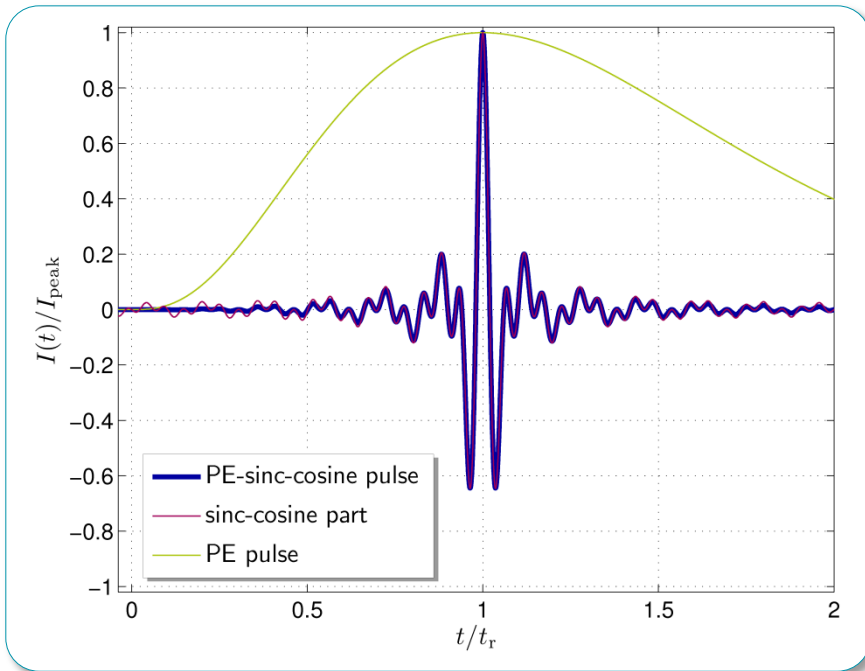
$$\begin{aligned} \mathcal{I}(\omega_i, \omega_f) &= \int_{\omega_i}^{\omega_f} \left[\exp(j\omega' t_r) \hat{P}(j\omega') \right] d\omega' \\ &= I_0 t_r \Gamma(\nu + 1) \exp(\nu) \int_{\omega_i}^{\omega_f} \frac{\exp(j\omega' t_r)}{(j t_r \omega' + \nu)^{\nu+1}} d\omega' \\ &= I_0 \left(\exp(\nu) \int_{t_r \omega_i}^{t_r \omega_f} \frac{\exp(j \xi)}{j \xi + \nu} d\xi + j \sum_{m=1}^{\nu} \left\{ \Gamma(m) [\exp(\alpha) \alpha^{-\nu+m-1}] \Big|_{\alpha_i}^{\alpha_f} \right\} \right) \end{aligned}$$

with $\alpha_i = j t_r \omega_i + \nu$ and $\alpha_f = j t_r \omega_f + \nu$

Prerequisites: exciting pulses

Power exponential modulated – sinc-cosine pulse

$$K_{SC} = 13, \nu = 3, B = 7.1 \text{ GHz}, f_c = 6.85 \text{ GHz} \quad \begin{matrix} f_l = 3.1 \text{ GHz} \\ f_h = 10.4 \text{ GHz} \end{matrix}$$



Prerequisites: radiated field

$$\mathbf{H}^T(\mathbf{X}, t) = \frac{A^T}{4\pi|\mathbf{X}|^3} \left\{ \Theta_H^{\text{NF}} \left[I^T(t') + \frac{|\mathbf{X}|}{c_0} \partial_t I^T(t') \right] + \Theta_H^{\text{FF}} \frac{|\mathbf{X}|^2}{c_0^2} \partial_t^2 I^T(t') \right\}$$

where:

– $t' = t - |\mathbf{X}|/c_0 =$ wave travel time retarded, time coordinate

– $\Theta_H^{\text{NF}} =$ near-field radiated field directional characteristic

$$\Theta_H^{\text{NF}}(\mathbf{i}_{A^T}, \boldsymbol{\Xi}) = 3(\boldsymbol{\Xi} \cdot \mathbf{i}_{A^T}) \boldsymbol{\Xi} - \mathbf{i}_{A^T}$$

– $\Theta_H^{\text{FF}} =$ far-field radiated field directional characteristic

$$\Theta_H^{\text{FF}}(\mathbf{i}_{A^T}, \boldsymbol{\Xi}) = (\boldsymbol{\Xi} \cdot \mathbf{i}_{A^T}) \boldsymbol{\Xi} - \mathbf{i}_{A^T}$$

Prerequisites: received signal

EM reciprocity theorem of the time-convolution type

➡ Thévenin circuit generator voltage in \mathcal{L}^R

$$V^G(\mathbf{X}, t') = -\frac{\mu_0 A^T A^R}{4\pi |\mathbf{X}|^3} \left\{ \Theta^{\text{NF}}(\mathbf{i}_{A^T}, \mathbf{i}_{A^R}, \mathbf{\Xi}) \left[\partial_t I^T(t') + \frac{|\mathbf{X}|}{c_0} \partial_t^2 I^T(t') \right] + \Theta^{\text{FF}}(\mathbf{i}_{A^T}, \mathbf{i}_{A^R}, \mathbf{\Xi}) \frac{|\mathbf{X}|^2}{c_0^2} \partial_t^3 I^T(t') \right\}$$

where:

– Θ^{NF} = near-field directional characteristic

$$\Theta^{\text{NF}}(\mathbf{i}_{A^T}, \mathbf{i}_{A^R}, \mathbf{\Xi}) = 3 (\mathbf{\Xi} \cdot \mathbf{i}_{A^T}) (\mathbf{\Xi} \cdot \mathbf{i}_{A^R}) - \mathbf{i}_{A^T} \cdot \mathbf{i}_{A^R}$$

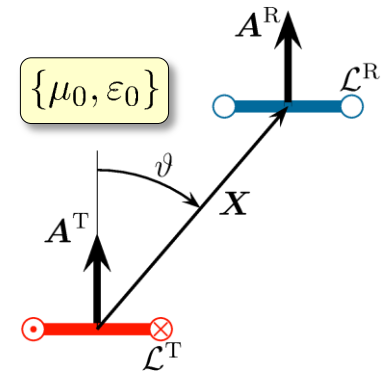
– Θ^{FF} = far-field directional characteristic

$$\Theta^{\text{FF}}(\mathbf{i}_{A^T}, \mathbf{i}_{A^R}, \mathbf{\Xi}) = (\mathbf{\Xi} \cdot \mathbf{i}_{A^T}) (\mathbf{\Xi} \cdot \mathbf{i}_{A^R}) - \mathbf{i}_{A^T} \cdot \mathbf{i}_{A^R}$$

Loop-to-loop transfer

Investigated canonical configurations

- Mutually parallel loops: $\mathbf{A}^T \cdot \mathbf{A}^R = A^T A^R$



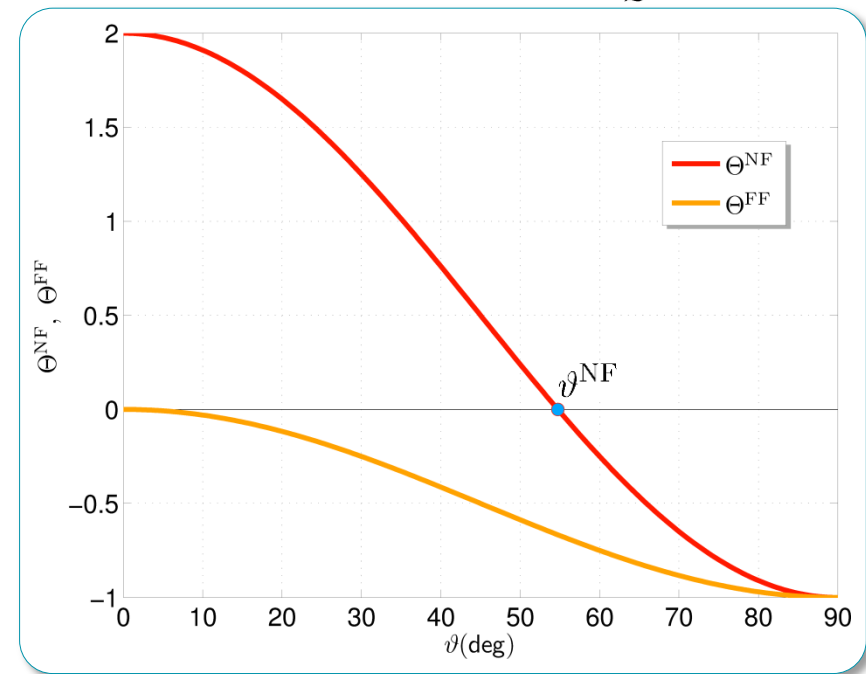
- Directional characteristics:

$$\Theta^{\text{NF}}(i_{\mathbf{A}^T}, i_{\mathbf{A}^R}, \Xi) = 3 \cos^2(\vartheta) - 1$$

$$\Theta^{\text{FF}}(i_{\mathbf{A}^T}, i_{\mathbf{A}^R}, \Xi) = \cos^2(\vartheta) - 1$$

zero
 $V^G(\mathbf{X}, t')$
 contributions

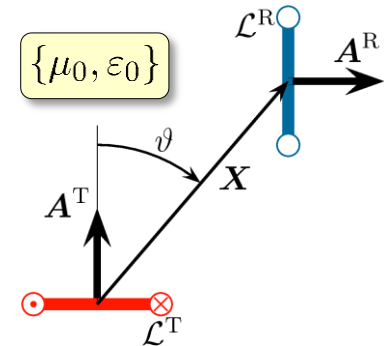
{	$\cos(\vartheta) = \pm 3^{-1/2}$	NF
	$\cos(\vartheta) = \pm 1$	FF



Loop-to-loop transfer

Investigated canonical configurations

- Mutually perpendicular loops: $\mathbf{A}^T \cdot \mathbf{A}^R = 0$



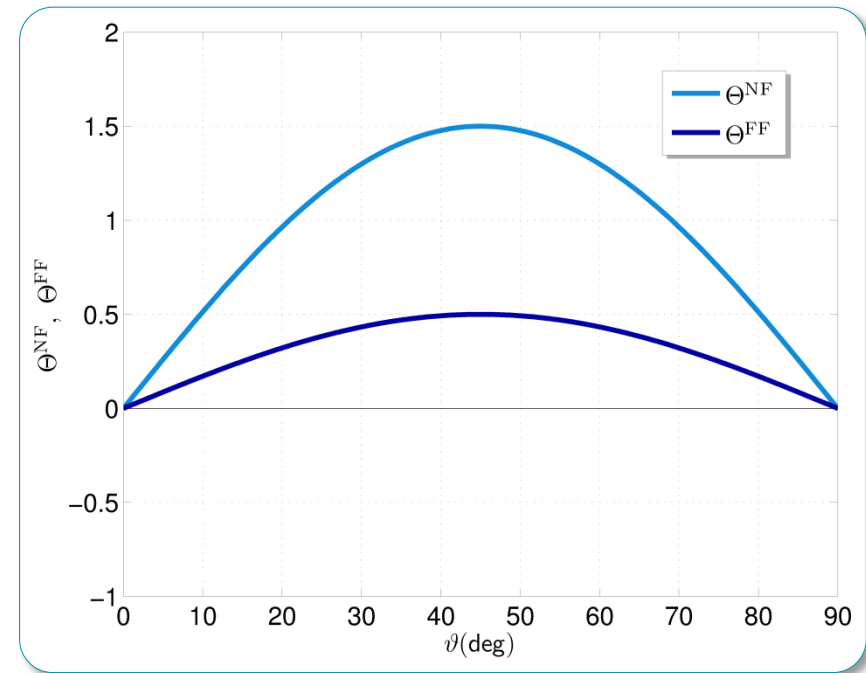
- Directional characteristics:

$$\Theta^{\text{NF}}(i_{A^T}, i_{A^R}, \Xi) = (3/2) \sin(2\vartheta) \sin(\varphi)$$

$$\Theta^{\text{FF}}(i_{A^T}, i_{A^R}, \Xi) = (1/2) \sin(2\vartheta) \sin(\varphi)$$


zero
 $V^G(\mathbf{X}, t')$
 contributions

{	$\varphi = \{0, \pi\}$	NF
	$\vartheta = \{0, \pi/2, \pi\}$	FF



Energy spectral density of emitted field

- International regulations on EMI:

- 
- a) Federal Communications Commission, "First Report and Order," April 2002.
 - b) National Telecommunications and Information Administration, "Manual of regulations and procedures for federal radio frequency management," May 2011 Revision of the 2008 Edition, [Online] Available: http://www.ntia.doc.gov/files/ntia/publications/manual_5_11.pdf.
 - c) Industry Canada, "Spectrum management and telecommunications. Radio standards specification. Devices using ultra-wideband (UWB) technology," RSS-220, Issue 1, March 2009.

power spectral density

- 
- Pulsed field → energy spectral density

Energy spectral density of emitted field

- International regulations on EMI: **far-field radiation**
- For loop-to-loop transfer

$$\{\mathbf{E}^T, \mathbf{H}^T\}(\mathbf{X}, t) = \frac{\{\mathbf{E}^{T;\infty}, \mathbf{H}^{T;\infty}\}(\boldsymbol{\Xi}, t - |\mathbf{X}|/c_0)}{4\pi|\mathbf{X}|} [1 + o(1)] \text{ as } |\mathbf{X}| \rightarrow \infty$$

where:

- $\mathbf{H}^{T;\infty}$ = far-field radiated magnetic field strength

$$\mathbf{H}^{T;\infty}(\boldsymbol{\Xi}, t) = A^T \boldsymbol{\Theta}_H^{\text{FF}} \frac{1}{c_0^2} \partial_t^2 I^T(t)$$

- $\mathbf{E}^{T;\infty}$ = far-field radiated electric field strength

$$\mathbf{E}^{T;\infty}(\boldsymbol{\Xi}, t) = (\mu_0/\epsilon_0)^{1/2} \mathbf{H}^{T;\infty}(\boldsymbol{\Xi}, t) \times \boldsymbol{\Xi}$$

Energy spectral density of emitted field

- The total energy radiated by the loop

$$W^{\text{rad}} = \left(\frac{1}{4\pi}\right)^2 \left(\frac{\mu_0}{\epsilon_0}\right)^{1/2} \int_{\Xi \in \Omega} d\Omega \int_{t=-\infty}^{\infty} |\mathbf{H}^{\text{T};\infty}(\Xi, t)|^2 dt$$



Parseval's theorem

$$W^{\text{rad}} = \int_{f=-\infty}^{\infty} w^{\text{rad}}(f) df = 2 \int_{f=0}^{\infty} w^{\text{rad}}(f) df$$

where:

- w^{rad} = energy spectral density

$$w^{\text{rad}}(f) = \left(\frac{1}{4\pi}\right)^2 \left(\frac{\mu_0}{\epsilon_0}\right)^{1/2} \int_{\Xi \in \Omega} |\hat{\mathbf{H}}^{\text{T};\infty}(\Xi, 2\pi jf)|^2 d\Omega$$

Energy spectral density of emitted field

- The total energy radiated by the loop

$$W^{\text{rad}}(f) = \frac{8\pi}{3} \left(\frac{A^{\text{T}}}{4\pi} \right)^2 \left(\frac{\mu_0}{\epsilon_0} \right)^{1/2} \frac{1}{c_0^4} \int_{t=0}^{\infty} [\partial_t^2 I(t)]^2 dt$$

- The energy spectral density

$$w^{\text{rad}}(f) = \frac{8\pi^3}{3} (A^{\text{T}})^2 \left(\frac{\mu_0}{\epsilon_0} \right)^{1/2} \frac{1}{c_0^4} f^4 |\hat{I}^{\text{T}}(2\pi j f)|^2$$

Numerical experiments

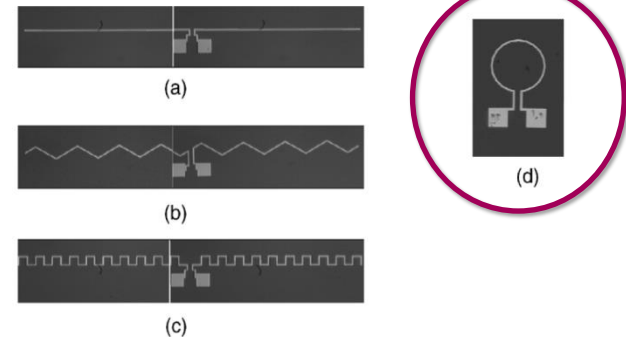
Loop-to-loop transfer

- Loops:

- $A^T = A^R = 0.0314 \text{ mm}^2$
- for circular loops $d = 0.2 \text{ mm}$

- Feeding pulse:

- pulse type: monocycle
- peak current: $I_{\text{peak}} = 1 \text{ mA}$
- pulse zero-crossing time: $t_{0x} = t_r = 0.1 \text{ ns}$

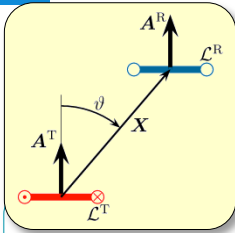


K.K. O, *et al.* "On-chip antennas in Silicon ICs and their application," *IEEE Trans. Electron Devices*, vol. 57, no. 1, pp. 1312–1321, July 2005.

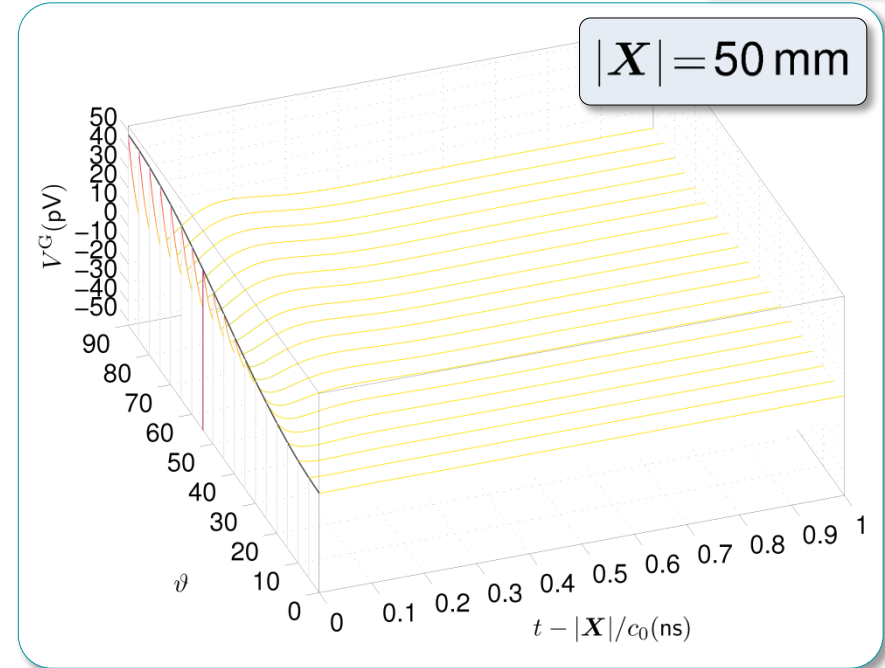
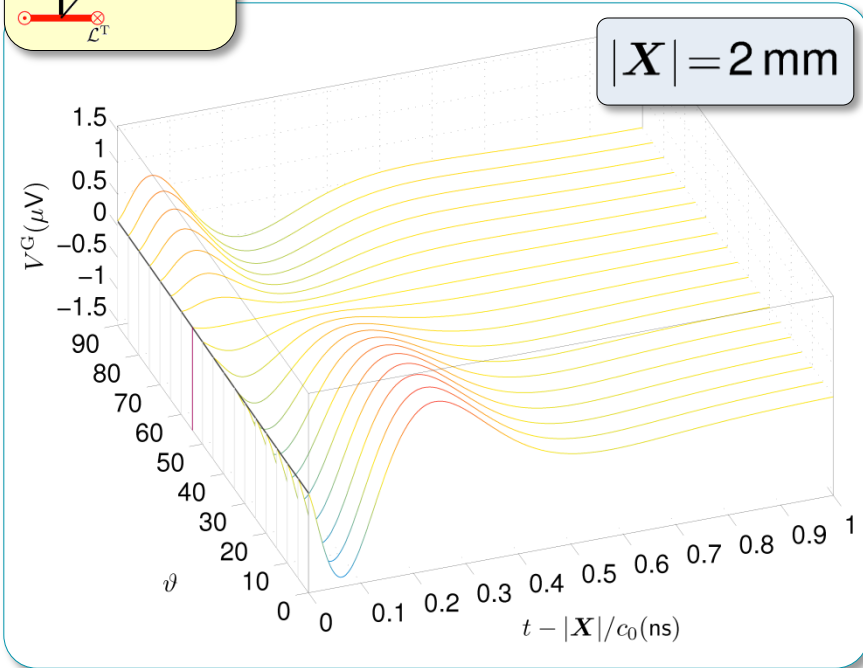
Numerical experiments

Loop-to-loop transfer

- strong NF signal + low FF signal
- intricate behaviour



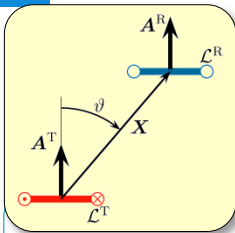
$\nu = 4$



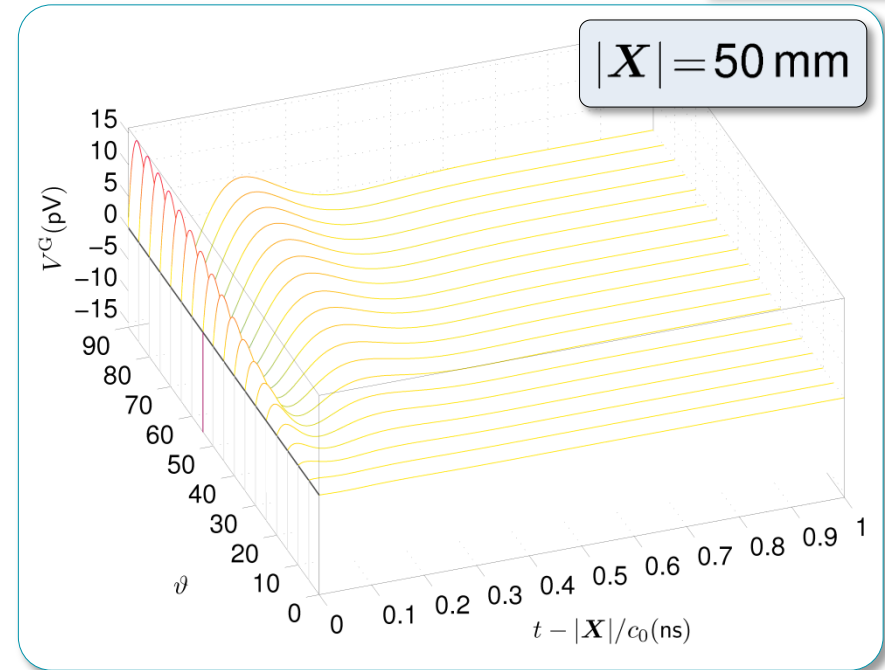
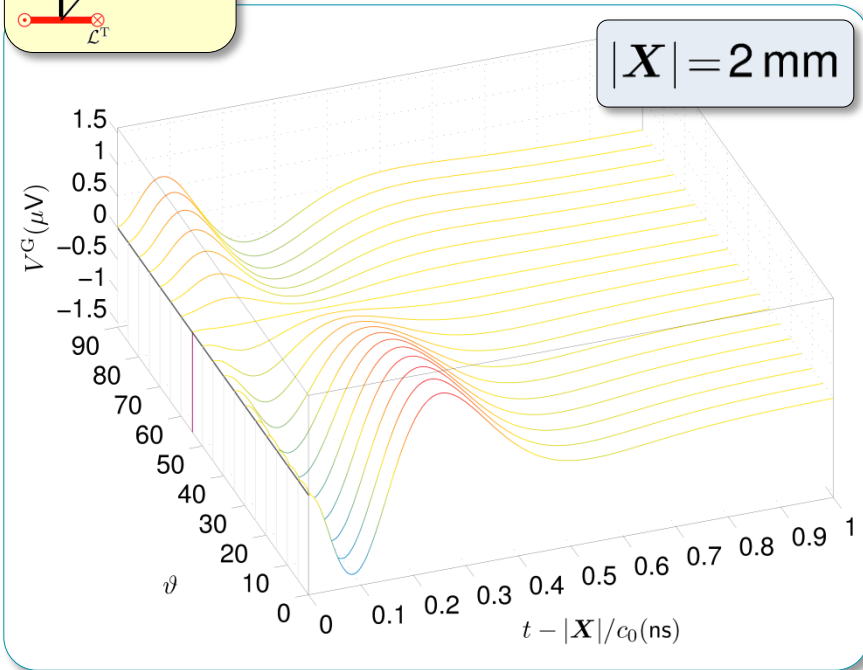
Numerical experiments

Loop-to-loop transfer

- strong NF signal + low FF signal
- intricate behaviour






$\nu = 5$



Numerical experiments

Loop-to-loop transfer

Practical implications:

- Highly idealised conditions
- Pulsed field loop-to-loop transfer  large potential to establish a viable intra-chip link
- Large NF/FF ratio  low EM contamination
- Already hint at the intricacy of the signal transfer  impact on the complexity of the signal processing

Numerical experiments

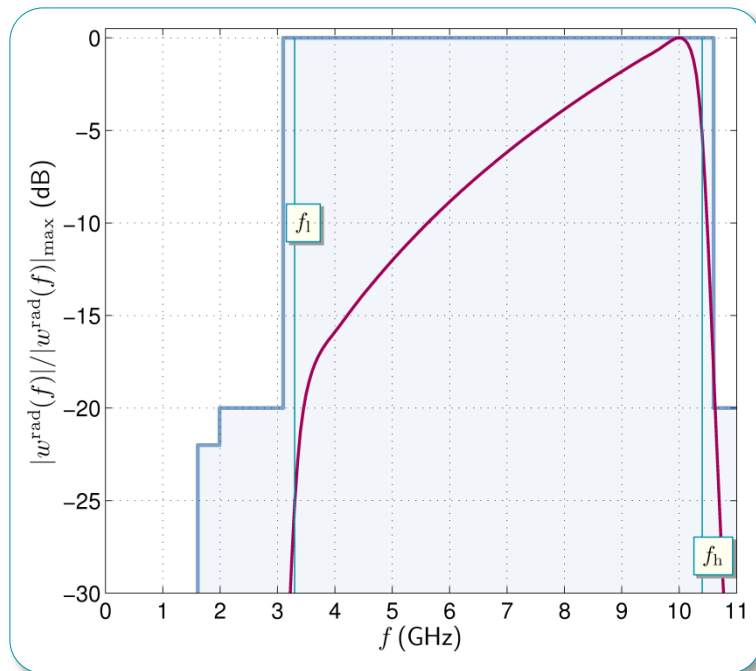
Energy spectral density analysis

- Transmitting loop:
 - same
- Feeding pulse:
 - Power exponential modulated – sinc-cosine pulse
 - Parameters: $K_{sc}=13$, $\nu=3$, $f_l=3.1$ GHz, $f_h=10.4$ GHz,
 $B=7.1$ GHz, $f_c=6.85$ GHz
- Reference behaviour: the FCC mask 3.1–10.6 GHz

Numerical experiments

Energy spectral density analysis

• Practical implications:



- Full compliance to the FCC mask
- Design strategy: determine I_0 for this pulse signature
- Verify the system functionality

Conclusions

- Pulsed transfer:
 - clear theoretical description
 - clear design rules
 - opportune system properties

- Pulsed-field wireless transfer has the potential of becoming the enabler of future digital data transfer technologies



Thank you